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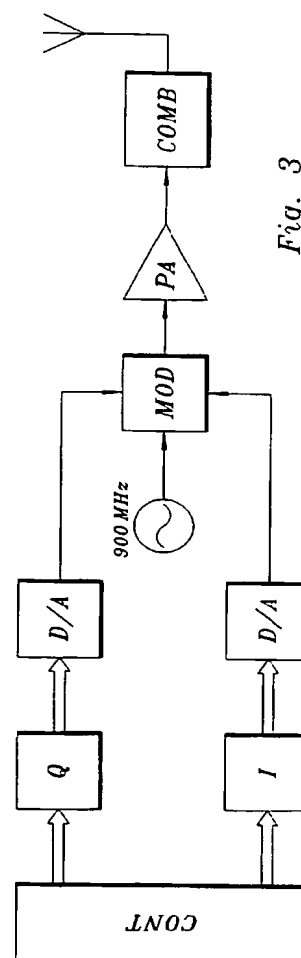
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(54) **Method of compensating the dependence of the useful transmitter signal on the transfer function of a combiner filter.**

(57) The invention relates to a method of compensating the dependence of the useful transmitter signal on the transfer function of a combiner filter in a mobile radio communication system. Before the useful transmitter signal is fed to the combiner filter it is filtered in the base band in connection with carrier frequency modulation with a filter, the total transfer function of which at least approximately comprises the inverted value of the transfer function of the combiner filter (COMB) transformed to the base band.



EP 0 518 835 A1

## TECHNICAL FIELD

The present invention relates to a method of compensating the dependence of the useful transmitter signal on the transfer function of a combiner filter in a mobile radio communication system.

## BACKGROUND OF THE INVENTION

Combiner filters, usually of cavity or dielectric type, are used to connect output signals from several power amplifiers and with different frequencies to a common antenna. The combiner filters are tuned to the frequencies that are used in the respective power amplifiers. Since the transfer functions of the combiner filters are not ideally rectangular unacceptable phase and amplitude distortion of the signal that passes through a combiner filter can arise. As an example the frequency dependant group delay in the combiner filter induces a phase error. Furthermore, the non-constant amplitude response within the modulation band width generates an amplitude pulsation. This means in particular that single pole filters cannot be used if a very large channel distance, that allows wide filters, is not used.

## SUMMARY OF THE INVENTION

An object of the present invention is to provide a method of compensating the dependence of the useful transmitter signal on the transfer function of a combiner filter in a mobile radio communication system in such a way that the above phase and amplitude errors can be reduced or eliminated.

In accordance with the present invention this object is achieved filtering the useful transmitter signal in connection with carrier frequency modulation in the base band with a filter, the total transfer function of which at least approximately comprises the inverted value of the transfer function of the combiner filter (COMB) transformed to the base band.

## BRIEF DESCRIPTION OF THE DRAWINGS

The invention, together with further objects and advantages thereof, may best be understood by making reference to the following description taken together with the accompanying drawings, in which:

FIGURE 1 shows the transfer function of a distortion free combiner filter;

FIGURE 2 shows the transfer function of a single pole combiner filter;

FIGURE 3 shows an apparatus for performing a preferred embodiment of the method of the present invention.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Figure 1 diagrammatically shows the transfer function of a distortion free combiner filter. This distortion free filter is characterized in that it is a band pass filter with the amplification 1 within the pass band and the amplification 0 outside the pass band. Furthermore, the filter exhibits a phase shift that varies linearly with frequency (the dashed line in Fig. 1). Since the useful transmitter signal is frequency modulated the amplitude and/or phase shifts that correspond to frequency shifts within the pass band will not be distorted by such a distortion free combiner filter.

However, in practice it is not possible to obtain the distortion free combiner filter of Figure 1. Figure 2 shows the transfer function of a combiner filter that is often used in practise, namely a single pole filter. In this case the pass band will contain a varying amplification and also a phase shift that varies non linearly with frequency (represented by the dashed curve in Fig. 2). For this reason the frequency shifts corresponding to amplitude and/or phase shifts of the useful transmitter signal will lead to distortion of the modulated signal.

However, the distortion caused by the combiner filter is known since the transfer function of the filter is known. Therefore, in accordance with the basic idea of the invention, the distortion caused by the combiner filter can be compensated by filtering the transmitter signal before it is fed to the combiner filter, in a filter, the transfer function of which within the frequency range occupied by the transmitter signal at least approximately comprises the inverted value of the combiner filter transfer function within the same frequency range.

Figure 3 shows an apparatus for performing a preferred embodiment of the method of the invention.

A controller CONT in the transmitter feeds, in accordance with known phase modulation techniques (see for instance "Data for Engineers: Radio, Electronics, Computers and Communications", Howard W Sams & Co, Inc, p. 23-5, Fig. 6), blocks of digital signals that are to be recoded for modulation to two PROMs, that in Figure 3 are designated Q and I. The output signals from these PROMs correspond to a complex number, the phase

of which in this embodiment is used for phase modulation. These output signals are converted in respective D/A-converters and fed to a modulator MOD, which is also fed with a carrier signal with a frequency of the order of for instance 900 MHz. The modulated signal is fed to a power amplifier PA and thereafter to the combiner filter COMB and finally to the antenna. The system as described so far works in accordance with known principles.

One possibility to implement the basic idea of the invention would be to insert an inverted filter in accordance with the above between the modulator MOD and the combiner filter COMB. However, since a combiner filter has a transfer function with a narrow peak at a very high frequency (900 MHz in the example) such a solution is hard to implement. For this reason the transfer function of the combiner filter COMB is, in accordance with the invention, first transformed down to the base band of the useful signal. There it will resemble the transfer function of a low pass filter. If the inverted value of the transfer function of this low pass filter is calculated, the transfer function for a high pass filter is obtained. The unmodulated signal can therefore be fed through such a filter to compensate the distortion of the combiner filter.

A derivation of a compensating filter for compensation already in the base band follows below.

Assume that the combiner filter has the transfer function:

$$H_{comb}(j\omega) = \frac{j\omega \frac{\omega_c}{Q}}{(j\omega)^2 + j\omega \frac{\omega_c}{Q} + \omega_c^2}$$

where  $\omega$  is the angular frequency of the combiner signal,  $\omega_c$  is the angular frequency of the carrier and  $Q$  is the Q-value of the combiner filter. Typical values for  $\omega_c$  and  $Q$  are  $2\pi \cdot 900 \cdot 10^6$  rad/s and 2000, respectively.

Sought is a compensating filter with the transfer function  $H(j\omega_b)$  that has the same phase and amplitude properties as  $1/H_{comb}(j(\omega_b + \omega_c))$ , where  $\omega_b$  is the base band angular frequency. That is, the sought filter has a transfer function that is formed by the transfer function for the combiner filter transformed to the base band and thereafter inverted. Since in practice  $0 < \omega_b < 2\pi \cdot 200 \cdot 10^3$  rad/s this condition has to be fulfilled only within the given range. In the given example, considering that  $\omega_b \ll \omega_c$ :

$$\begin{aligned} H_b(j\omega_b) &= \frac{j(\omega_b + \omega_c) \frac{\omega_c}{Q}}{(j(\omega_b + \omega_c))^2 + j(\omega_b + \omega_c) \frac{\omega_c}{Q} + \omega_c^2} = \\ &= \frac{j \frac{\omega_c^2}{Q} (1 + \frac{\omega_b}{\omega_c})}{j \frac{\omega_c^2}{Q} (1 + \frac{\omega_b}{\omega_c}) - 2\omega_b \omega_c (1 + \frac{1}{2} \frac{\omega_b}{\omega_c})} \approx (\omega_b \ll \omega_c) \approx \\ &\approx \frac{j \frac{\omega_c}{Q}}{j \frac{\omega_c}{Q} - 2\omega_b} = \frac{1}{1 + 2jQ \frac{\omega_b}{\omega_c}} \end{aligned}$$

where  $H_b(j\omega_b)$  is the transfer function of the combiner filter transformed to the base band. The sought transfer function  $H(j\omega_b)$  can therefore be approximated with:

$$H(j\omega_b) = 1 + 2jQ \frac{\omega_b}{\omega_c}$$

In a preferred embodiment this high pass filter can be implemented by modifying the coding tables I, Q of the carrier modulation in such a way that the filter function is simulated already in the modulation coding (it is to be noted that  $Q$  here designates a table and is not to be confused with the Q-value of the filter mentioned above). In this case no further hardware is required. These coding tables are defined in non-corrected form as:

$$\begin{aligned} I(t) &= \cos(\varphi(t)) \\ Q(t) &= \sin(\varphi(t)) \end{aligned}$$

where  $\varphi(t)$  is defined for instance in accordance with European standard GSM 05.04 section 2.5. An example

of sampled tables for I,Q can be found at the end of this specification. One row in these tables represents 8 samples during one bit time. The controller CONT chooses one of the 64 rows for each new bit depending on the quadrant in which the modulation is located and on the data content of the new bit and the three last bits. This procedure is standardized and is not an object of this invention.

The above functions are now to be corrected in such a way that the distortion of the combiner filter is compensated. For this reason the instantaneous frequency deviation of the useful signal is defined according to:

$$\omega_f(t) = \frac{d\varphi(t)}{dt}$$

Furthermore, the group delay distortion of the combiner filter as a function of the angular frequency is defined as:

$$G_d(\omega) = -\frac{d}{d\omega} \arg[H_{comb}(j\omega)]$$

By the substitution

$$\omega = \omega_c + \omega_f(t)$$

this group delay distortion can be expressed as a function of t, that is as  $G_d(t)$ . The phase error generated by the combiner filter is thereafter transformed to the base band according to:

$$\varphi_{dist}(t) = 2\pi G_d(t) \omega_f(t)$$

The amplitude error generated by a combiner filter is calculated according to the formula:

$$A_{dist}(t) = \text{abs}[H_{comb}(\omega_c + \omega_f(t))]$$

Using the above expressions the tables for the corrected I- and Q-values can now be calculated according to:

$$I_{corr}(t) = \frac{\cos[\varphi(t) - \varphi_{dist}(t)]}{A_{dist}(t)}$$

$$Q_{corr}(t) = \frac{\sin[\varphi(t) - \varphi_{dist}(t)]}{A_{dist}(t)}$$

Corrected tables corresponding to the above mentioned tables for I,Q can be found at the end of this specification. These tables generate a correction for the above exemplified combiner filter.

Due to the general form of these correction formulas the correction can also be performed in two steps. First a phase correction is performed in the IQ-modulation step. In this case the amplitude correction is performed in the transmitter instead, suitably as late as possible in the same, preferably in the final stage itself. The reason for this is that a normal transmitter often contains several more or less saturated amplifier stages, which would eliminate or reduce the amplitude correction that has been added in the IQ-modulation step. Preferably a final stage with variable amplification that is controlled by the signal  $1/A_{dist}(t)$  is used. In this embodiment the I,Q-tables which are only phase corrected, are given by:

$$I_{corr}(t) = \cos[\varphi(t) - \varphi_{dist}(t)]$$

$$Q_{corr}(t) = \sin[\varphi(t) - \varphi_{dist}(t)]$$

It is appreciated that the method in accordance with the invention can also be used with multiple pole filters, although the necessity for compensation is less since such filters have a transfer function that is flatter near the central frequency of the filter.

It will be understood by those skilled in the art that various modifications and changes may be made to the present invention without departure from the spirit and scope thereof, which is defined by the appended claims.

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40	7.6483e-001	6.7373e-001	5.9620e-001	5.4463e-001	5.2727e-001	5.4691e-001	6.0040e-001	6.7917e-001
35	7.0512e-001	6.3716e-001	5.7600e-001	5.3457e-001	5.2281e-001	5.4521e-001	5.9992e-001	6.7917e-001
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25	6.3722e-001	5.0949e-001	3.5452e-001	1.7954e-001	-5.8449e-003	-1.9089e-001	-3.6488e-001	-5.1833e-001
20	6.3713e-001	5.0918e-001	3.5359e-001	1.7707e-001	-1.1726e-002	-2.0351e-001	-3.8932e-001	-5.6103e-001
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10	-6.3722e-001	-5.0949e-001	-3.5452e-001	-1.7954e-001	5.8449e-003	1.9089e-001	3.6488e-001	5.1833e-001
5	-7.0503e-001	-6.3687e-001	-5.7519e-001	-5.3245e-001	-5.1778e-001	-5.3437e-001	-5.7860e-001	-6.4108e-001
	-7.0512e-001	-6.3716e-001	-5.7600e-001	-5.3457e-001	-5.2281e-001	-5.4521e-001	-5.9992e-001	-6.7917e-001
	-7.6483e-001	-6.7373e-001	-5.9620e-001	-5.4463e-001	-5.2727e-001	-5.4691e-001	-6.0040e-001	-6.7917e-001
	-7.6475e-001	-6.7346e-001	-5.9540e-001	-5.4252e-001	-5.2226e-001	-5.3608e-001	-5.7909e-001	-6.4108e-001
	-7.0262e-001	-5.5057e-001	-3.7772e-001	-1.9127e-001	6.0168e-004	1.8889e-001	3.6433e-001	5.1833e-001
	-7.0253e-001	-5.5026e-001	-3.7680e-001	-1.8881e-001	6.4830e-003	2.0152e-001	3.8877e-001	5.6103e-001
	-7.1165e-001	-8.3499e-001	-9.2629e-001	-9.8201e-001	-9.9998e-001	-9.7948e-001	-9.2133e-001	-8.2779e-001
	-7.1157e-001	-8.3479e-001	-9.2592e-001	-9.8154e-001	-1.0000e+000	-9.8200e-001	-9.3127e-001	-8.5518e-001
	-6.4433e-001	-7.3922e-001	-8.0343e-001	-8.4004e-001	-8.5279e-001	-8.4417e-001	-8.1526e-001	-7.6748e-001
	-6.4423e-001	-7.3897e-001	-8.0283e-001	-8.3868e-001	-8.4970e-001	-8.3719e-001	-7.9970e-001	-7.3398e-001
	7.0909e-001	7.7074e-001	8.1745e-001	8.4512e-001	8.5245e-001	8.3830e-001	8.0006e-001	7.3398e-001
	7.0918e-001	7.7097e-001	8.1802e-001	8.4646e-001	8.5551e-001	8.4525e-001	8.1561e-001	7.6748e-001
	7.7068e-001	8.6048e-001	9.3505e-001	9.8375e-001	9.9998e-001	9.8161e-001	9.3105e-001	8.5518e-001



55	7.7076e-001	8.6066e-001	9.3540e-001	9.8420e-001	9.9993e-001	9.7907e-001	9.2110e-001	8.2779e-001
	7.7076e-001	8.6066e-001	9.3540e-001	9.8420e-001	9.9993e-001	9.7907e-001	9.2110e-001	8.2779e-001
	7.7068e-001	8.6048e-001	9.3505e-001	9.8375e-001	9.9998e-001	9.8161e-001	9.3105e-001	8.5518e-001
	7.0918e-001	7.7097e-001	8.1802e-001	8.4646e-001	8.5551e-001	8.4525e-001	8.1561e-001	7.6748e-001
	7.0909e-001	7.7074e-001	8.1745e-001	8.4512e-001	8.5245e-001	8.3830e-001	8.0006e-001	7.3398e-001
	-6.4423e-001	-7.3897e-001	-8.0283e-001	-8.3868e-001	-8.4970e-001	-8.3719e-001	-7.9970e-001	-7.3398e-001
	-6.4433e-001	-7.3922e-001	-8.0343e-001	-8.4004e-001	-8.5279e-001	-8.4417e-001	-8.1526e-001	-7.6748e-001
	-7.1157e-001	-8.3479e-001	-9.2592e-001	-9.8154e-001	-1.0000e+000	-9.8200e-001	-9.3127e-001	-8.5518e-001
	-7.1165e-001	-8.3499e-001	-9.2629e-001	-9.8201e-001	-9.9998e-001	-9.7948e-001	-9.2133e-001	-8.2779e-001
	-7.0253e-001	-5.5026e-001	-3.7680e-001	-1.8881e-001	6.4830e-003	2.0152e-001	3.8877e-001	5.6103e-001
	-7.0262e-001	-5.5057e-001	-3.7772e-001	-1.9127e-001	6.0168e-004	1.8889e-001	3.6433e-001	5.1833e-001
	-7.6475e-001	-6.7346e-001	-5.9540e-001	-5.4252e-001	-5.2226e-001	-5.3608e-001	-5.7909e-001	-6.4108e-001
	-7.6483e-001	-6.7373e-001	-5.9620e-001	-5.4463e-001	-5.2727e-001	-5.4691e-001	-6.0040e-001	-6.7917e-001
	-7.0512e-001	-6.3716e-001	-5.7600e-001	-5.3457e-001	-5.2281e-001	-5.4521e-001	-5.9992e-001	-6.7917e-001
	-7.0503e-001	-6.3687e-001	-5.7519e-001	-5.3245e-001	-5.1778e-001	-5.3437e-001	-5.7860e-001	-6.4108e-001
	-6.3722e-001	-5.0949e-001	-3.5452e-001	-1.7954e-001	5.8449e-003	1.9089e-001	3.6488e-001	5.1833e-001
	-6.3713e-001	-5.0918e-001	-3.5359e-001	-1.7707e-001	1.1726e-002	2.0351e-001	3.8932e-001	5.6103e-001
	6.3713e-001	5.0918e-001	3.5359e-001	1.7707e-001	-1.1726e-002	-2.0351e-001	-3.8932e-001	-5.6103e-001
	6.3722e-001	5.0949e-001	3.5452e-001	1.7954e-001	-5.8449e-003	-1.9089e-001	-3.6488e-001	-5.1833e-001
	7.0503e-001	6.3687e-001	5.7519e-001	5.3245e-001	5.1778e-001	5.3437e-001	5.7860e-001	6.4108e-001
	7.0512e-001	6.3716e-001	5.7600e-001	5.3457e-001	5.2281e-001	5.4521e-001	5.9992e-001	6.7917e-001
	7.6483e-001	6.7373e-001	5.9620e-001	5.4463e-001	5.2727e-001	5.4691e-001	6.0040e-001	6.7917e-001
	7.6475e-001	6.7346e-001	5.9540e-001	5.4252e-001	5.2226e-001	5.3608e-001	5.7909e-001	6.4108e-001
	7.0262e-001	5.5057e-001	3.7772e-001	1.9127e-001	-6.0168e-004	-1.8889e-001	-3.6433e-001	-5.1833e-001

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7.0253e-001 5.5026e-001 3.7680e-001 1.8881e-001 -6.4830e-003 -2.0152e-001 -3.8877e-001 -5.6103e-001  
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7.1165e-001 8.3499e-001 9.2629e-001 9.8201e-001 9.9998e-001 9.7948e-001 9.2133e-001 8.2779e-001

55	-7.6138e-001	-8.8612e-001	-9.7686e-001	-1.0301e+000	-1.0436e+000	-1.0171e+000	-9.5137e-001	-8.4915e-001
50	-7.6121e-001	-8.8571e-001	-9.7598e-001	-1.0285e+000	-1.0418e+000	-1.0168e+000	-9.5787e-001	-8.7363e-001
45	-6.6852e-001	-7.5537e-001	-8.1150e-001	-8.4230e-001	-8.5281e-001	-8.4525e-001	-8.1886e-001	-7.7284e-001
40	-6.6837e-001	-7.5501e-001	-8.1072e-001	-8.4072e-001	-8.4970e-001	-8.3891e-001	-8.0506e-001	-7.4207e-001
35	7.1846e-001	7.7896e-001	8.2216e-001	8.4634e-001	8.5247e-001	8.4014e-001	8.0538e-001	7.4179e-001
30	7.1858e-001	7.7927e-001	8.2288e-001	8.4784e-001	8.5551e-001	8.4645e-001	8.1921e-001	7.7271e-001
25	7.9606e-001	8.9503e-001	9.7550e-001	1.0259e+000	1.0397e+000	1.0158e+000	9.5778e-001	8.7402e-001
20	7.9619e-001	8.9538e-001	9.7630e-001	1.0273e+000	1.0415e+000	1.0161e+000	9.5136e-001	8.4978e-001
15	7.9662e-001	8.9580e-001	9.7662e-001	1.0275e+000	1.0415e+000	1.0158e+000	9.5089e-001	8.4910e-001
10	7.9648e-001	8.9544e-001	9.7583e-001	1.0260e+000	1.0397e+000	1.0156e+000	9.5740e-001	8.7357e-001
5	7.1879e-001	7.7943e-001	8.2296e-001	8.4787e-001	8.5551e-001	8.4647e-001	8.1930e-001	7.7287e-001
	7.1867e-001	7.7912e-001	8.2224e-001	8.4636e-001	8.5247e-001	8.4018e-001	8.0552e-001	7.4211e-001
	-6.6786e-001	-7.5470e-001	-8.1058e-001	-8.4068e-001	-8.4970e-001	-8.3887e-001	-8.0492e-001	-7.4176e-001
	-6.6801e-001	-7.5506e-001	-8.1136e-001	-8.4226e-001	-8.5281e-001	-8.4523e-001	-8.1878e-001	-7.7267e-001
	-7.6043e-001	-8.8510e-001	-9.7558e-001	-1.0284e+000	-1.0418e+000	-1.0170e+000	-9.5825e-001	-8.7409e-001
	-7.6059e-001	-8.8551e-001	-9.7645e-001	-1.0299e+000	-1.0437e+000	-1.0173e+000	-9.5185e-001	-8.4983e-001
	-7.1442e-001	-5.5221e-001	-3.6873e-001	-1.7101e-001	3.3321e-002	2.3635e-001	4.3024e-001	6.0753e-001
	-7.1451e-001	-5.5257e-001	-3.6989e-001	-1.7424e-001	2.5386e-002	2.1901e-001	3.9638e-001	5.4831e-001
	-7.7626e-001	-6.7993e-001	-5.9855e-001	-5.4353e-001	-5.2227e-001	-5.3691e-001	-5.8281e-001	-6.4845e-001
	-7.7632e-001	-6.8018e-001	-5.9931e-001	-5.4556e-001	-5.2727e-001	-5.4834e-001	-6.0689e-001	-6.9427e-001
	-7.1043e-001	-6.4108e-001	-5.7815e-001	-5.3520e-001	-5.2282e-001	-5.4685e-001	-6.0676e-001	-6.9471e-001
	-7.1035e-001	-6.4082e-001	-5.7738e-001	-5.3314e-001	-5.1778e-001	-5.3535e-001	-5.8257e-001	-6.4871e-001
	-6.4474e-001	-5.1237e-001	-3.4966e-001	-1.6567e-001	2.8055e-002	2.1914e-001	3.9564e-001	5.4744e-001

I<sub>corr</sub>

55	-6.4465e-001	-5.1203e-001	-3.4855e-001	-1.6252e-001	3.5861e-002	2.3630e-001	4.2927e-001	6.0638e-001
50	6.4412e-001	5.1128e-001	3.4762e-001	1.6147e-001	-3.6974e-002	-2.3741e-001	-4.3032e-001	-6.0732e-001
45	6.4421e-001	5.1163e-001	3.4875e-001	1.6464e-001	-2.9120e-002	-2.2016e-001	-3.9654e-001	-5.4815e-001
40	7.1014e-001	6.4062e-001	5.7726e-001	5.3311e-001	5.1778e-001	5.3531e-001	5.8244e-001	6.4852e-001
35	7.1022e-001	6.4088e-001	5.7803e-001	5.3516e-001	5.2282e-001	5.4679e-001	6.0657e-001	6.9438e-001
30	7.7676e-001	6.8052e-001	5.9950e-001	5.4561e-001	5.2727e-001	5.4839e-001	6.0708e-001	6.9460e-001
25	7.7670e-001	6.8027e-001	5.9874e-001	5.4359e-001	5.2228e-001	5.3695e-001	5.8293e-001	6.4864e-001
20	7.1536e-001	5.5356e-001	3.7097e-001	1.7536e-001	-2.4273e-002	-2.1797e-001	-3.9548e-001	-5.4759e-001
15	7.1527e-001	5.5320e-001	3.6982e-001	1.7216e-001	-3.2161e-002	-2.3522e-001	-4.2918e-001	-6.0659e-001
10	7.6138e-001	8.8612e-001	9.7686e-001	1.0301e+000	1.0436e+000	1.0171e+000	9.5137e-001	8.4915e-001
5	7.6121e-001	8.8571e-001	9.7598e-001	1.0285e+000	1.0418e+000	1.0168e+000	9.5787e-001	8.7363e-001
	6.6852e-001	7.5537e-001	8.1150e-001	8.4230e-001	8.5281e-001	8.4525e-001	8.1886e-001	7.7284e-001
	6.6837e-001	7.5501e-001	8.1072e-001	8.4072e-001	8.4970e-001	8.3891e-001	8.0506e-001	7.4207e-001
	-7.1846e-001	-7.7896e-001	-8.2216e-001	-8.4634e-001	-8.5247e-001	-8.4014e-001	-8.0538e-001	-7.4179e-001
	-7.1858e-001	-7.7927e-001	-8.2288e-001	-8.4784e-001	-8.5551e-001	-8.4645e-001	-8.1921e-001	-7.7271e-001
	-7.9606e-001	-8.9503e-001	-9.7550e-001	-1.0259e+000	-1.0397e+000	-1.0158e+000	-9.5778e-001	-8.7402e-001
	-7.9619e-001	-8.9538e-001	-9.7630e-001	-1.0273e+000	-1.0415e+000	-1.0161e+000	-9.5136e-001	-8.4978e-001
	-7.9662e-001	-8.9580e-001	-9.7662e-001	-1.0275e+000	-1.0415e+000	-1.0158e+000	-9.5089e-001	-8.4910e-001
	-7.9648e-001	-8.9544e-001	-9.7583e-001	-1.0260e+000	-1.0397e+000	-1.0156e+000	-9.5740e-001	-8.7357e-001
	-7.1879e-001	-7.7943e-001	-8.2296e-001	-8.4787e-001	-8.5551e-001	-8.4647e-001	-8.1930e-001	-7.7287e-001
	-7.1867e-001	-7.7912e-001	-8.2224e-001	-8.4636e-001	-8.5247e-001	-8.4018e-001	-8.0552e-001	-7.4211e-001
	6.6786e-001	7.5470e-001	8.1058e-001	8.4068e-001	8.4970e-001	8.3887e-001	8.0492e-001	7.4176e-001
	6.6801e-001	7.5506e-001	8.1136e-001	8.4226e-001	8.5281e-001	8.4523e-001	8.1878e-001	7.7267e-001
	7.6043e-001	8.8510e-001	9.7558e-001	1.0284e+000	1.0418e+000	1.0170e+000	9.5825e-001	8.7409e-001

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7.6059e-001	8.8551e-001	9.7645e-001	1.0299e+000	1.0437e+000	1.0173e+000	9.5185e-001	8.4983e-001
7.1442e-001	5.5221e-001	3.6873e-001	1.7101e-001	-3.3321e-002	-2.3635e-001	-4.3024e-001	-6.0753e-001
7.1451e-001	5.5257e-001	3.6989e-001	1.7424e-001	-2.5386e-002	-2.1901e-001	-3.9638e-001	-5.4831e-001
7.7626e-001	6.7993e-001	5.9855e-001	5.4353e-001	5.2227e-001	5.3691e-001	5.8281e-001	6.4845e-001
7.7632e-001	6.8018e-001	5.9931e-001	5.4556e-001	5.2727e-001	5.4834e-001	6.0689e-001	6.9427e-001
7.1043e-001	6.4108e-001	5.7815e-001	5.3520e-001	5.2282e-001	5.4685e-001	6.0676e-001	6.9471e-001
7.1035e-001	6.4082e-001	5.7738e-001	5.3314e-001	5.1778e-001	5.3535e-001	5.8257e-001	6.4871e-001
6.4474e-001	5.1237e-001	3.4966e-001	1.6567e-001	-2.8055e-002	-2.1914e-001	-3.9564e-001	-5.4744e-001
6.4465e-001	5.1203e-001	3.4855e-001	1.6252e-001	-3.5861e-002	-2.3630e-001	-4.2927e-001	-6.0638e-001
-6.4412e-001	-5.1128e-001	-3.4762e-001	-1.6147e-001	3.6974e-002	2.3741e-001	4.3032e-001	6.0732e-001
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45	7.7626e-001	6.7993e-001	5.9855e-001	5.4353e-001	5.2227e-001	5.3691e-001	5.8281e-001	6.4845e-001
40	7.7632e-001	6.8018e-001	5.9931e-001	5.4556e-001	5.2727e-001	5.4834e-001	6.0689e-001	6.9427e-001
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Q<sub>corr</sub>

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	7.9662e-001	8.9580e-001	9.7662e-001	1.0275e+000	1.0415e+000	1.0158e+000	9.5089e-001	8.4910e-001
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## Claims

1. A method of compensating the dependence of the useful transmitter signal on the transfer function of a combiner filter in a mobile radio communication system, **characterized in** that the useful transmitter signal in connection with carrier frequency modulation is filtered in the base band with a filter, the total transfer function of which at least approximately comprises the inverted value of the transfer function of the combiner filter (COMB) transformed to the base band.
2. The method of claim 1, **characterized in** that the coding tables (I,Q) of the carrier modulation are modified such that the filtering is performed in the modulation step itself.
3. The method of claim 1, **characterized in** that the useful transmitter signal before the carrier modulation is filtered in the base band with a first filter section, the transfer function of which has a constant amplitude and a phase that at least approximately comprises the sign reversed value of the phase of the combiner filter (COMB) transfer function transformed to the base band, and in that the transmitter output signal is filtered with a second filter section, the transfer function of which has constant phase and an amplitude that at least approximately comprises the inverted value of the amplitude of the combiner filter (COMB) transfer function.
4. The method of claim 3, **characterized in** that the coding tables (I,Q) of the carrier modulation are modified such that the first filter section is implemented in the modulation step itself.
5. The method of claim 3 or 4, **characterized in** that the second filter section is implemented by controlling the amplification of the final stage of the transmitter.
7. The method of any of the preceeding claims, **characterized in** that the combiner filter is a single pole filter.

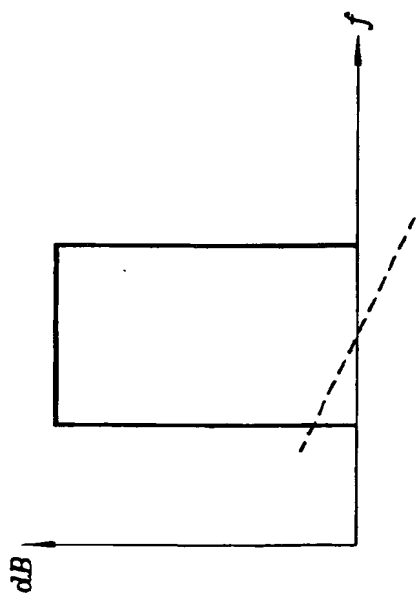


Fig. 1

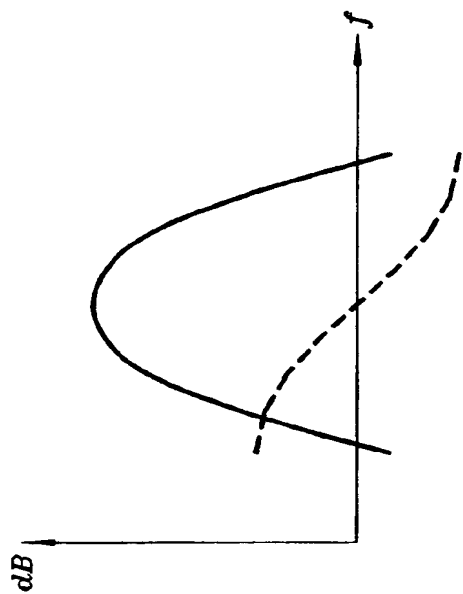


Fig. 2

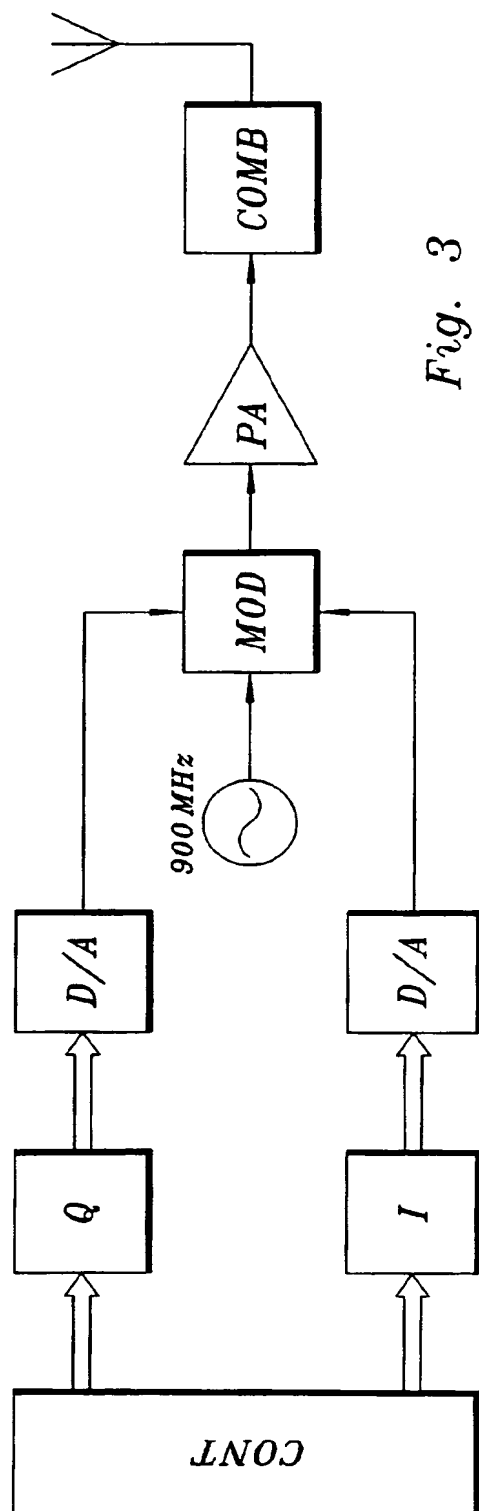


Fig. 3



European Patent  
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## EUROPEAN SEARCH REPORT

Application Number

EP 92850118.8

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	US-A- 4 890 300 (C.J. ANDREWS) *claim 1*	1-6	H 04 B 7/01 H 04 B 1/62 H 01 P 1/213
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A	US-A- 4 238 855 (R.W. ZBOROWSKI) *column 1, line 59 - line 68*	1-6	
	--		
A	US-A- 4 667 172 (LONGSHORE ET AL)	1-6	
	--		
A	US-A- 4 868 810 (VARY ET AL)	1-6	
	--		
A	US-A- 4 910 481 (SASAKI ET AL)	1-6	
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			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			H 04 B H 01 P
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
STOCKHOLM		01-09-1992	HOLMBERG. A.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

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